

## **6. OFFSHORE WIND TURBINES: FROM FIXED-BOTTOM TO FLOATING TECHNOLOGIES**

**6.1 Introduction**

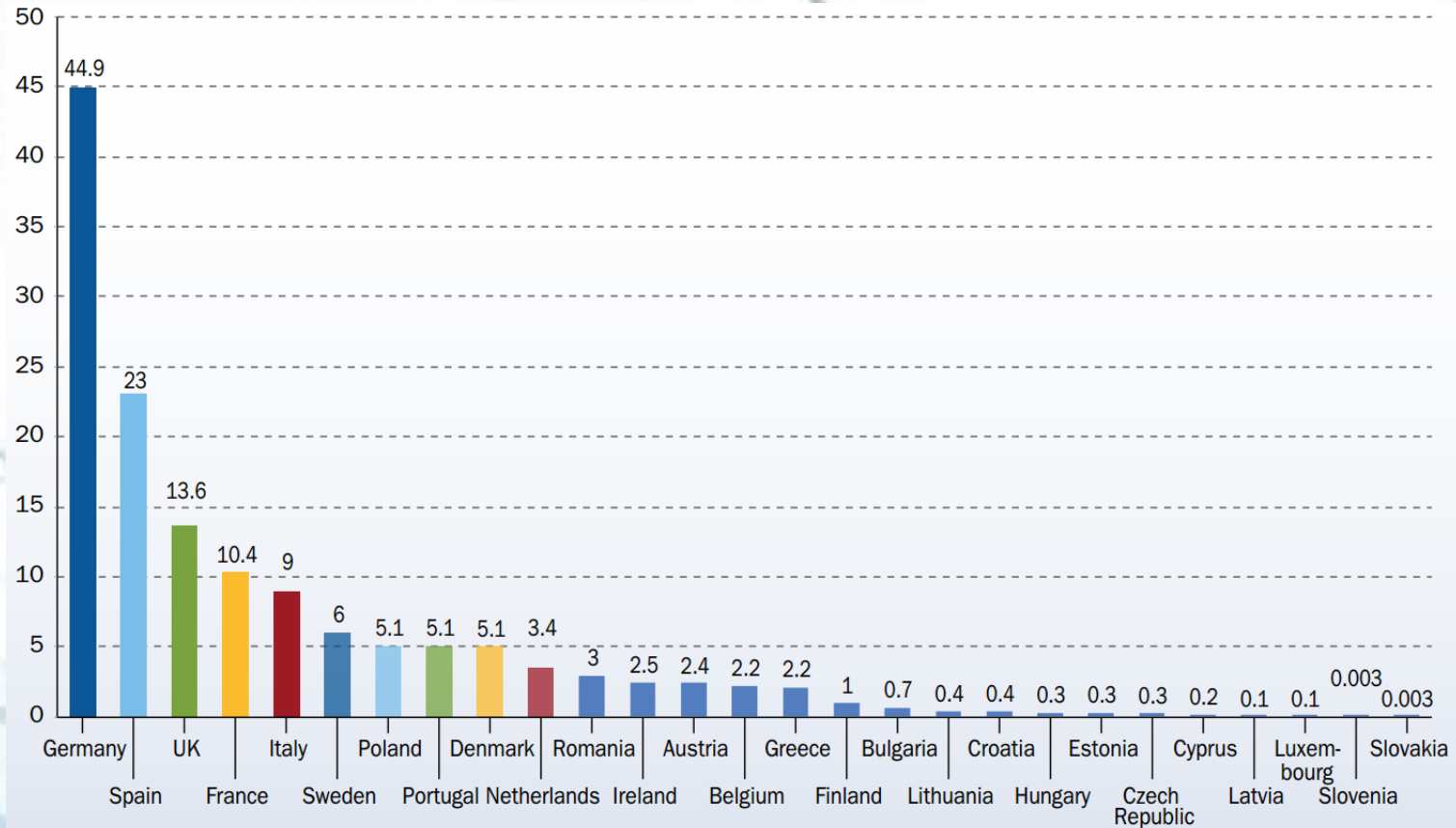
**6.2 Fixed-bottom technologies**

**6.3 Floating technologies**

**6.4 Conclusions**

## Introduction

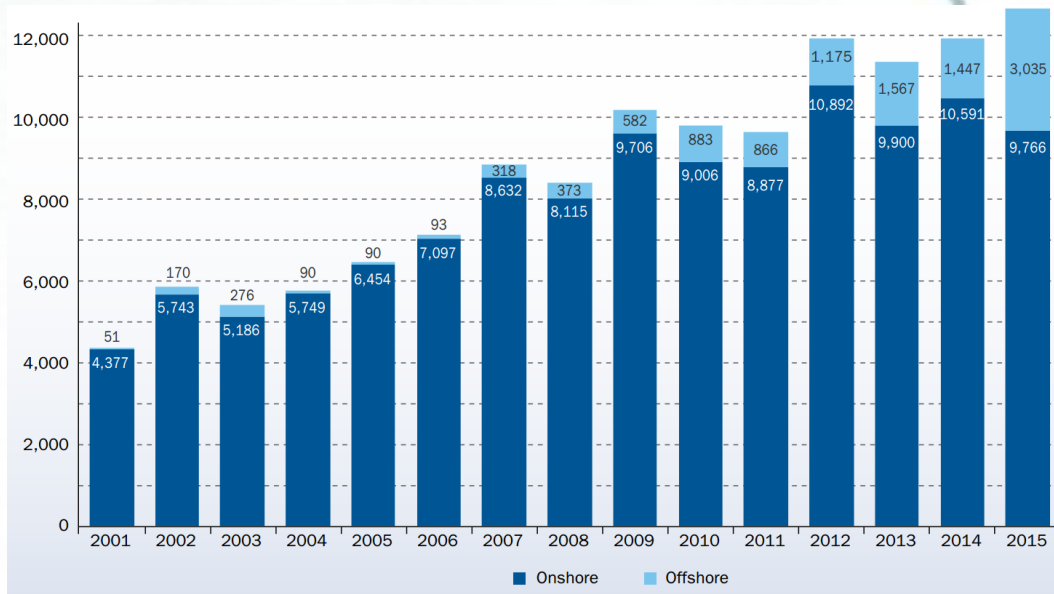
### The wind energy in Europe



EU member state market shares for total installed capacity (GW). Total 141.6 GW [source: EWEA, 2016]

## Fixed-bottom technologies

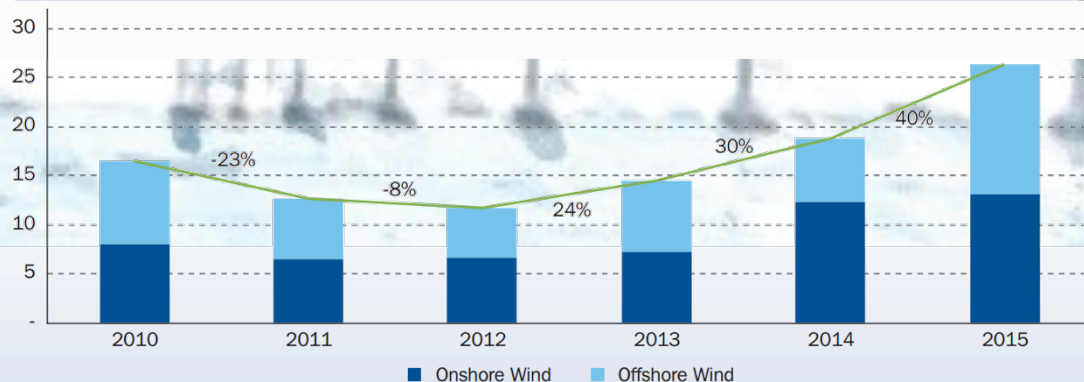
### Onshore and offshore wind energy in Europe



- Increase of offshore installations
- Increase of offshore investments

**Annual onshore and offshore installations (MW).**

[source: EWEA, 2016]



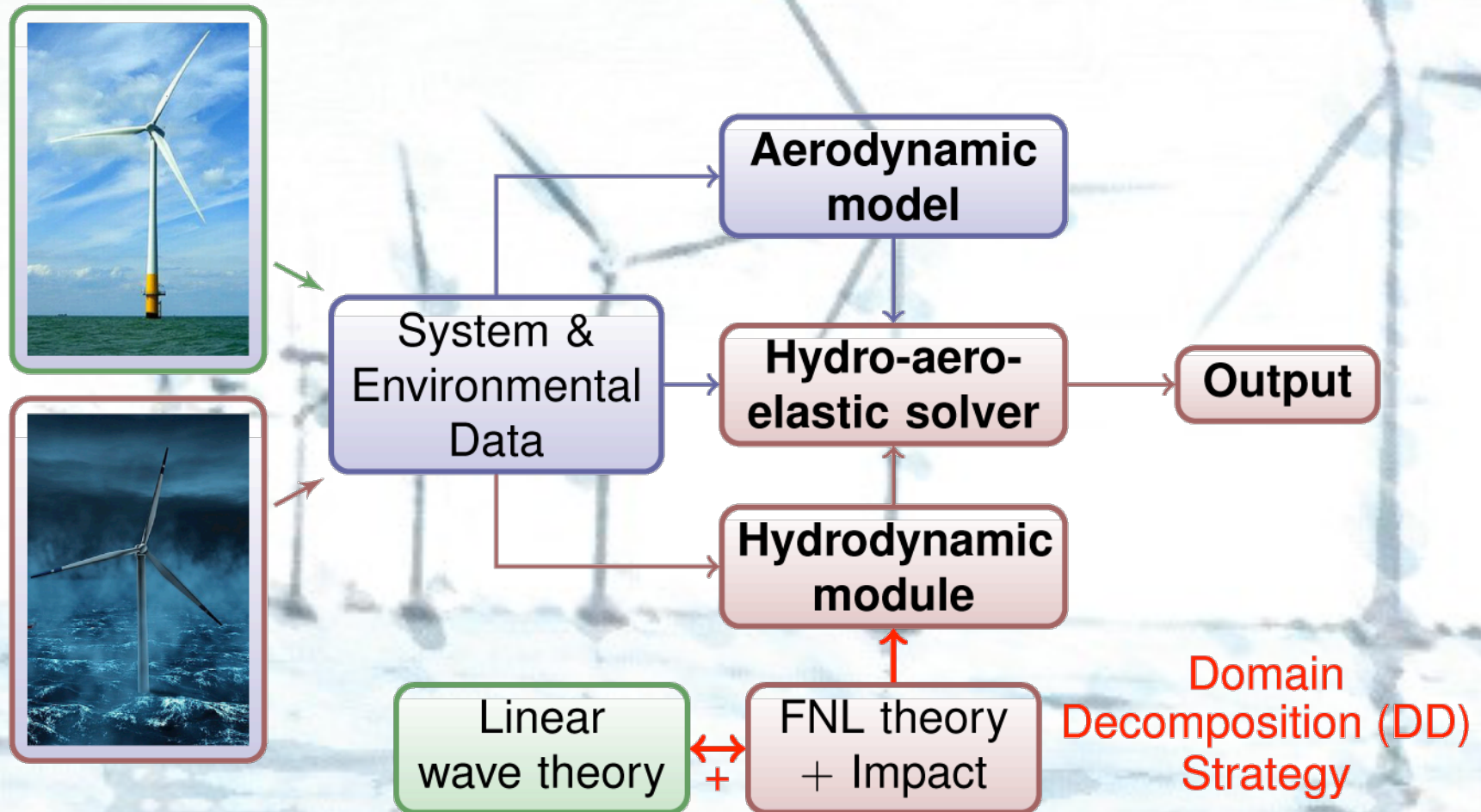
**Total annual investments in wind energy 2010-2015.**  
**Figures include investments in new assets (€ BN).**

[source: EWEA, 2016]



# Fixed-bottom technologies

## Proposed methodology to account for nonlinear waves





# Proposed simulation scheme

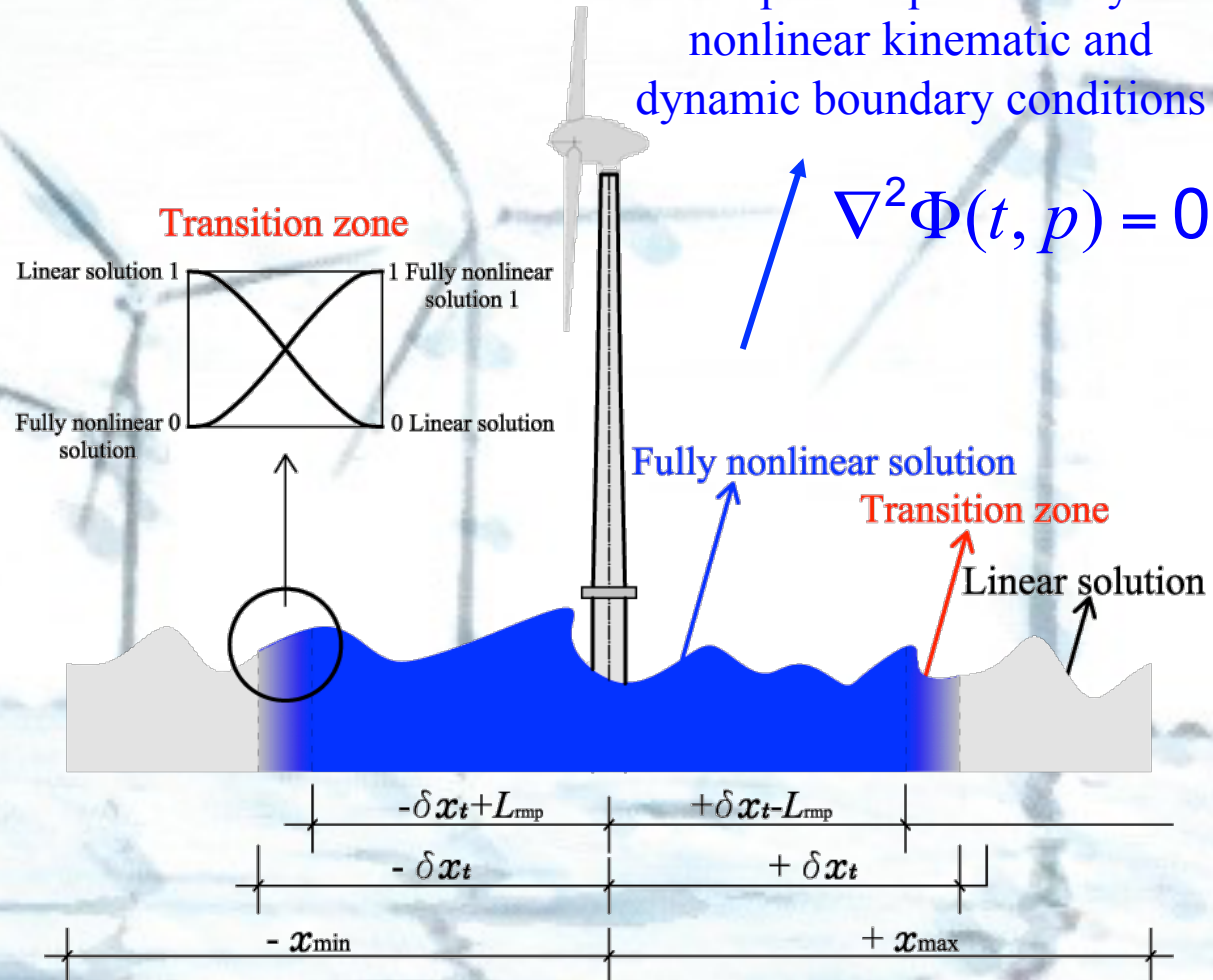
## Linear–Nonlinear transition scheme

Efficient transition zone:

- Eulerian to Lagrangian description (and v.v.)
- Linear to nonlinear solution (and v.v.)

It assures:

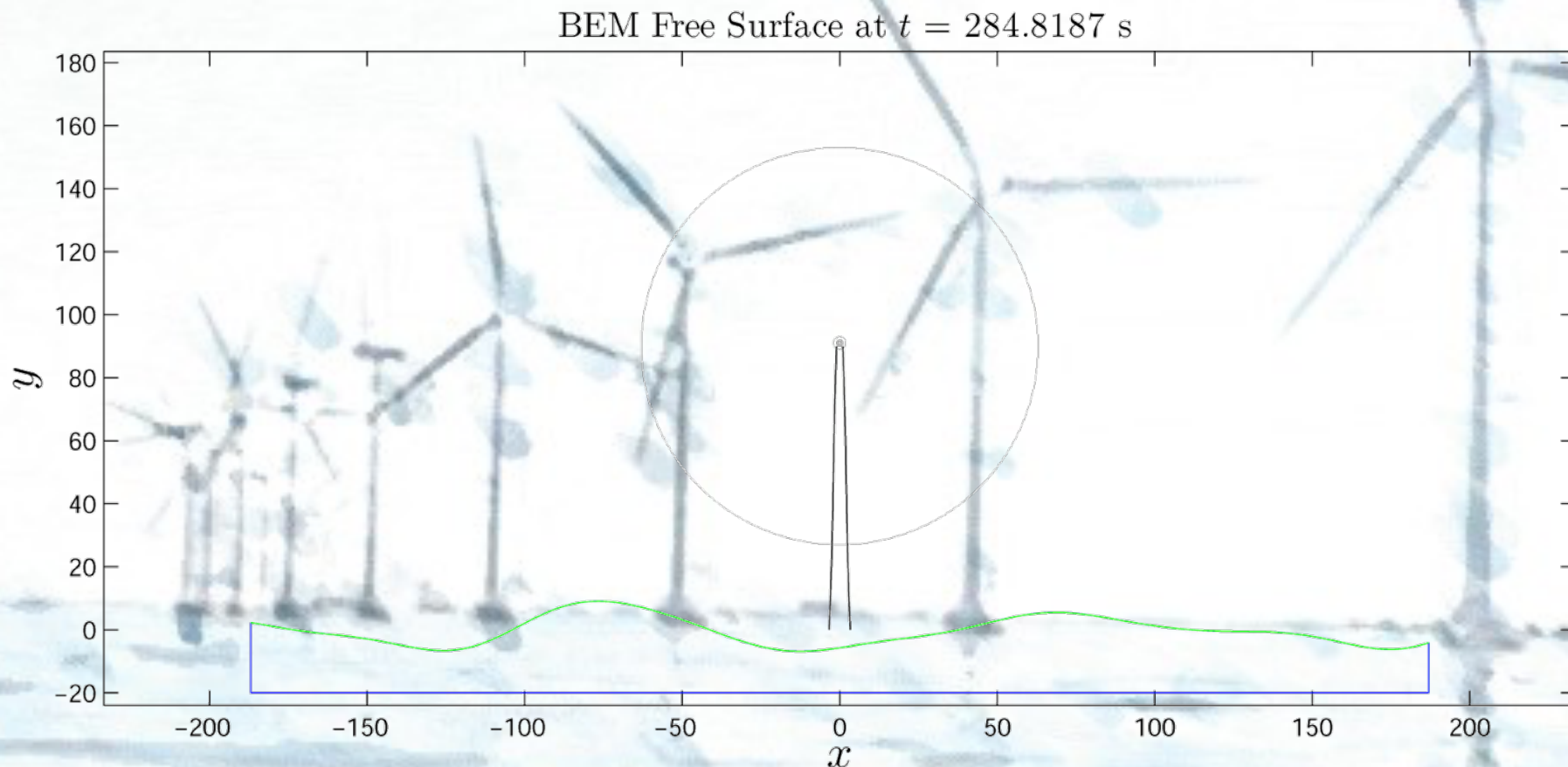
- No reflection
- Long simulations



Potential flow model (non-viscous, irrotational):  
Laplace eq. with fully nonlinear kinematic and dynamic boundary conditions

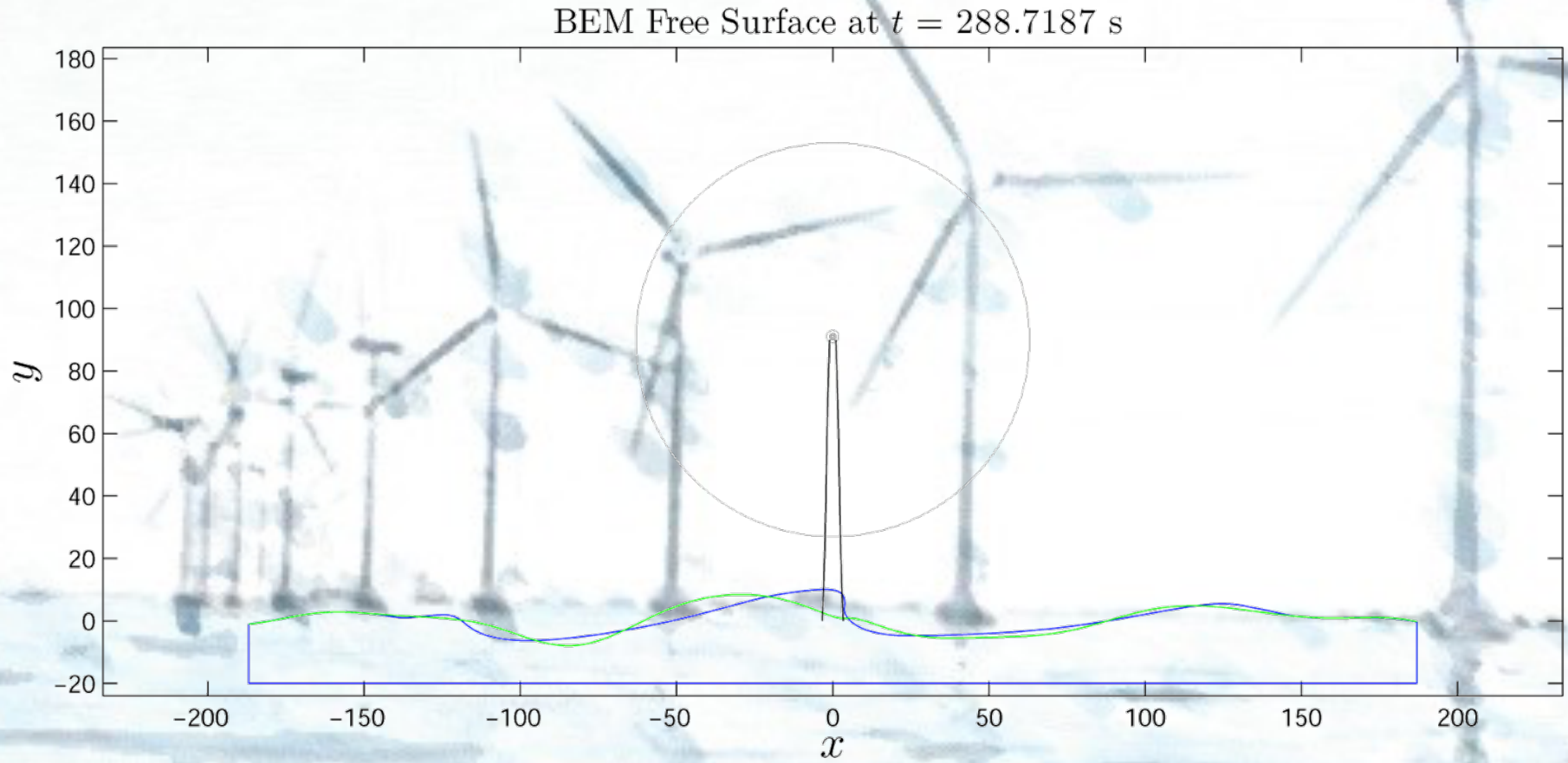
## Proposed simulation scheme

### Example: L vs. FNL breaking wave propagation I



# Proposed simulation scheme

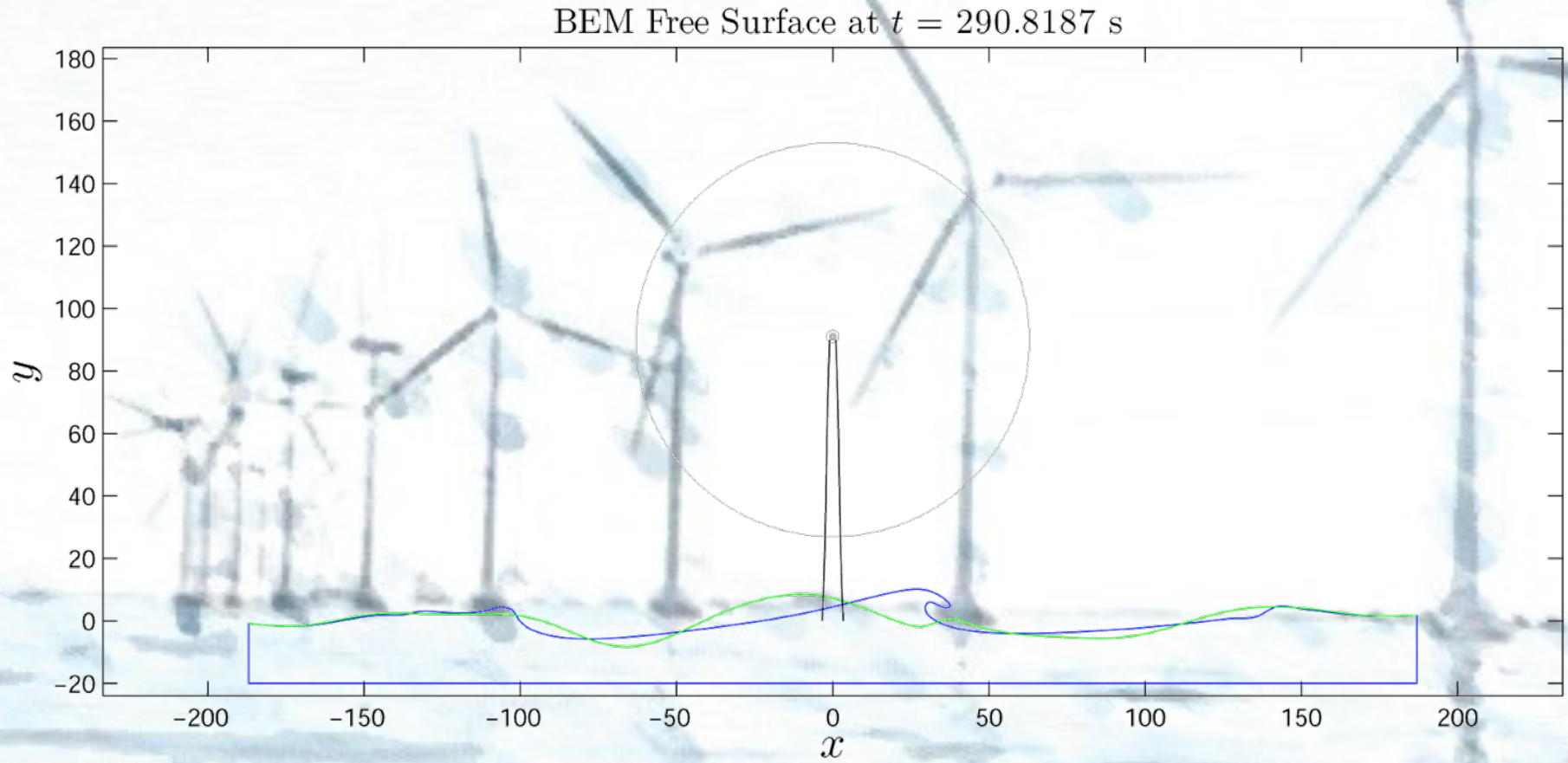
## Example: L vs. FNL breaking wave propagation II





# Proposed simulation scheme

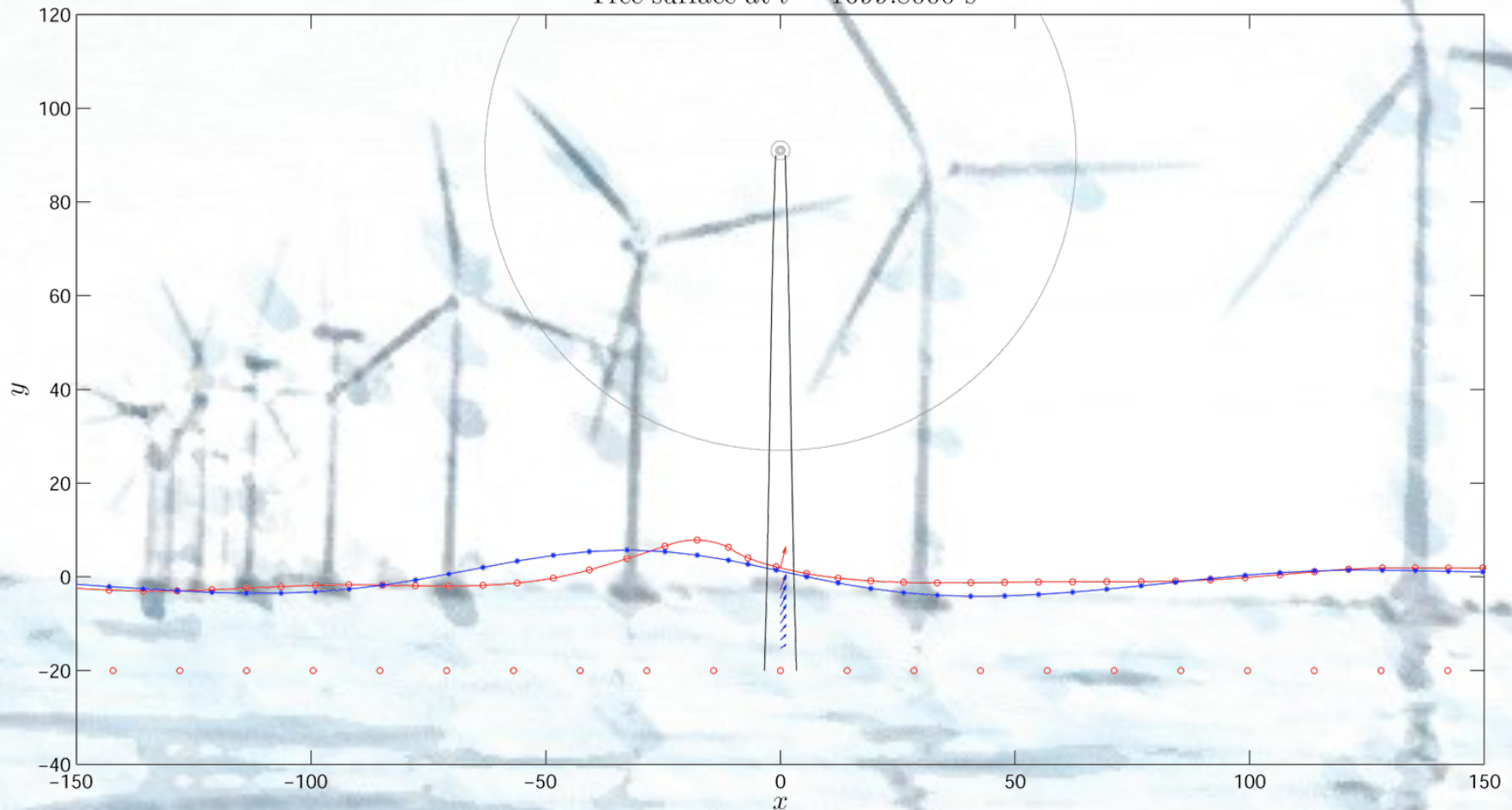
## Example: L vs. FNL breaking wave propagation III



## Proposed simulation scheme

### Example: L vs. FNL non-breaking wave propagation I

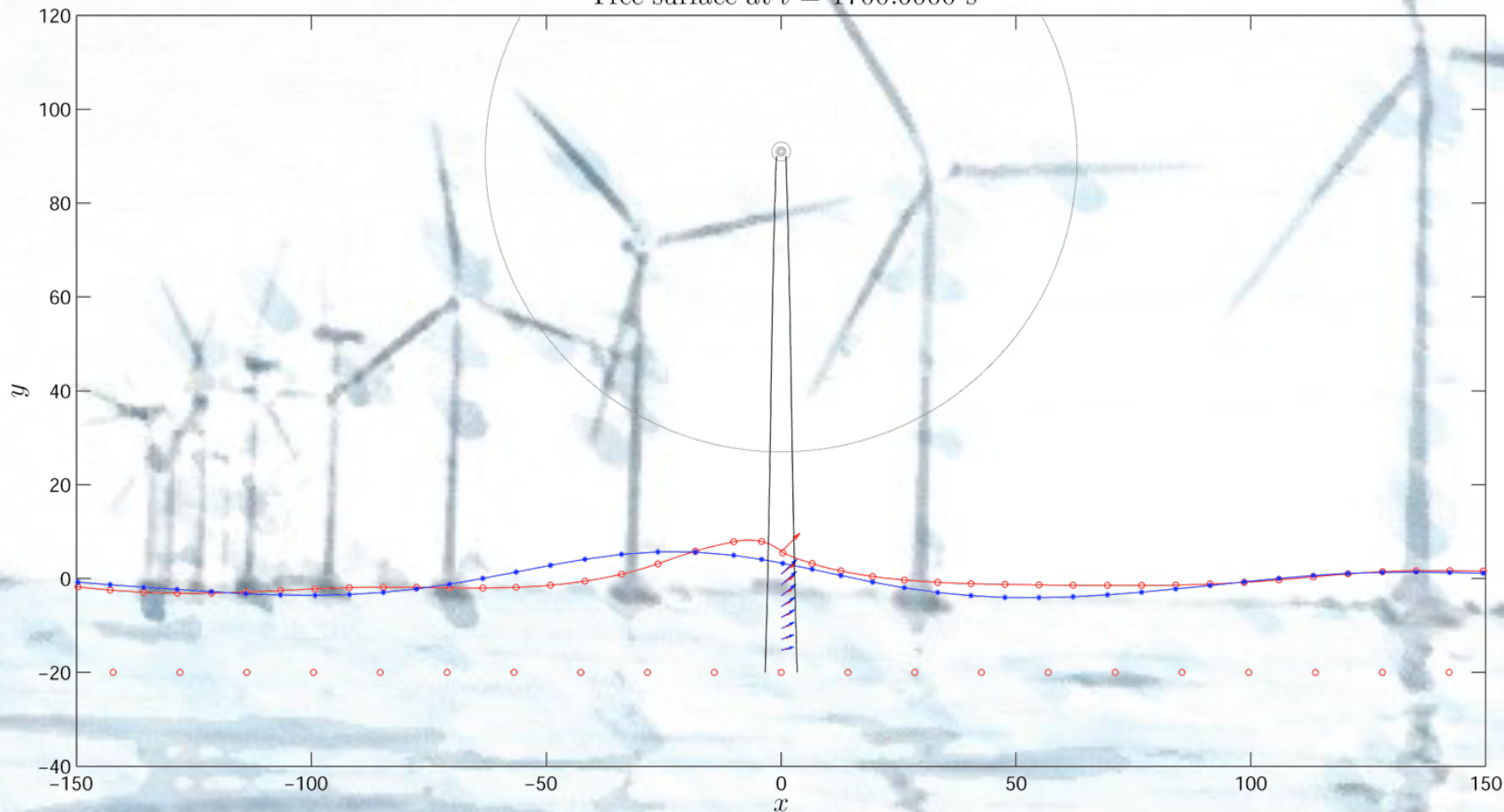
Free surface at  $t = 1699.8000$  s



## Proposed simulation scheme

### Example: L vs. FNL non-breaking wave propagation II

Free surface at  $t = 1700.6000$  s

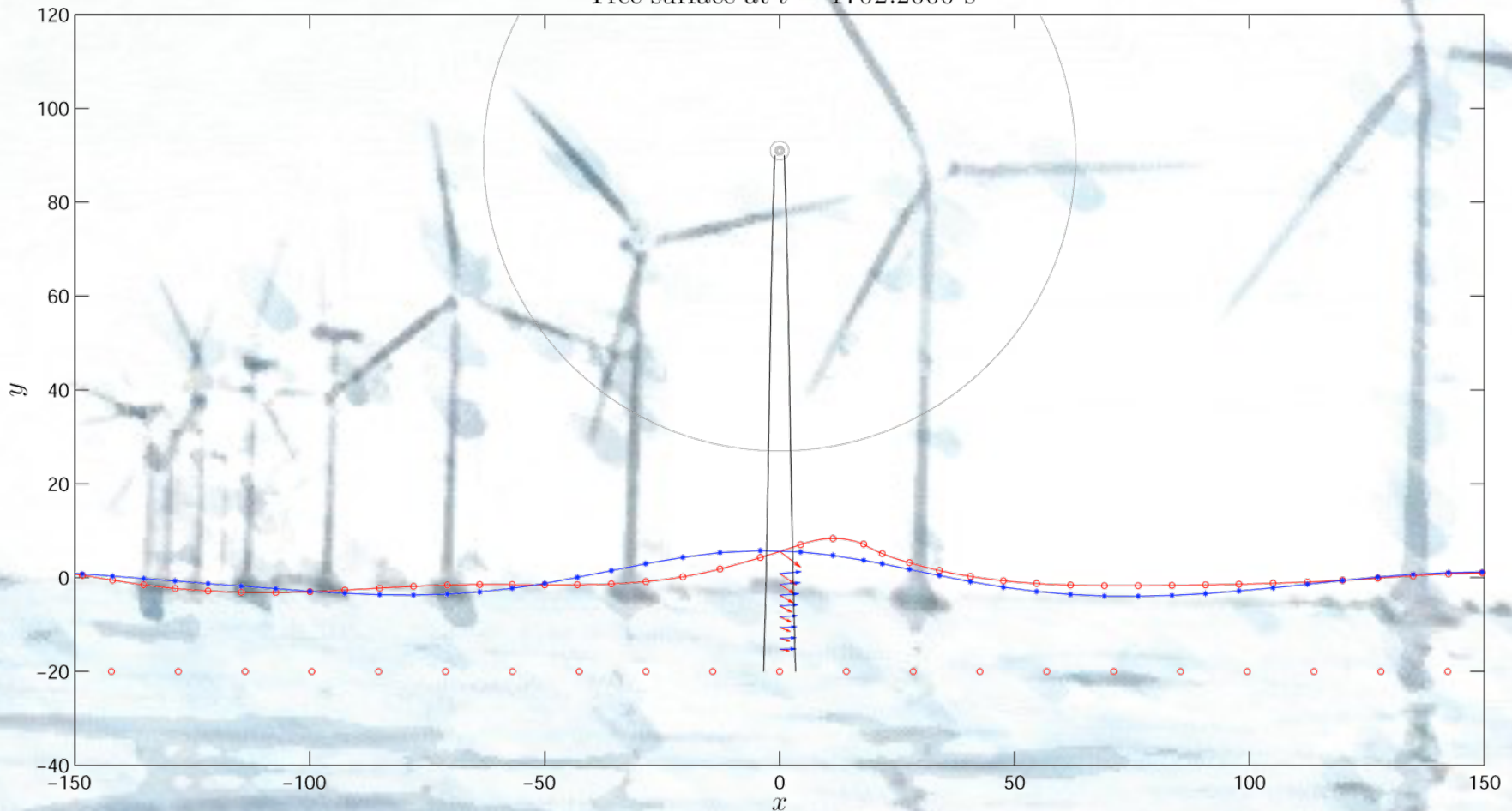




## Proposed simulation scheme

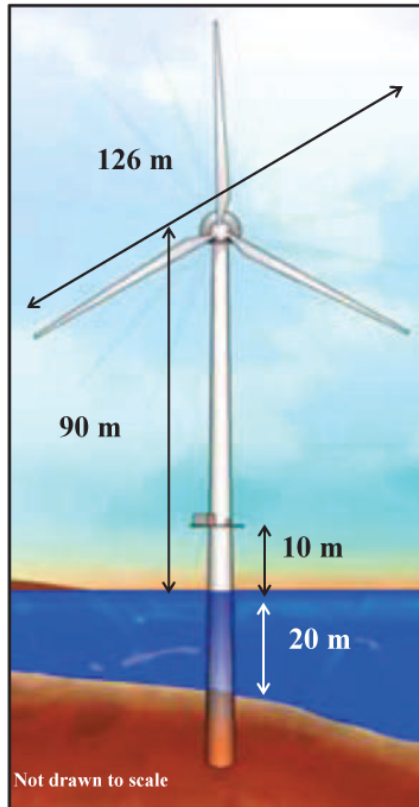
### Example: L vs. FNL non-breaking wave propagation III

Free surface at  $t = 1702.2000$  s

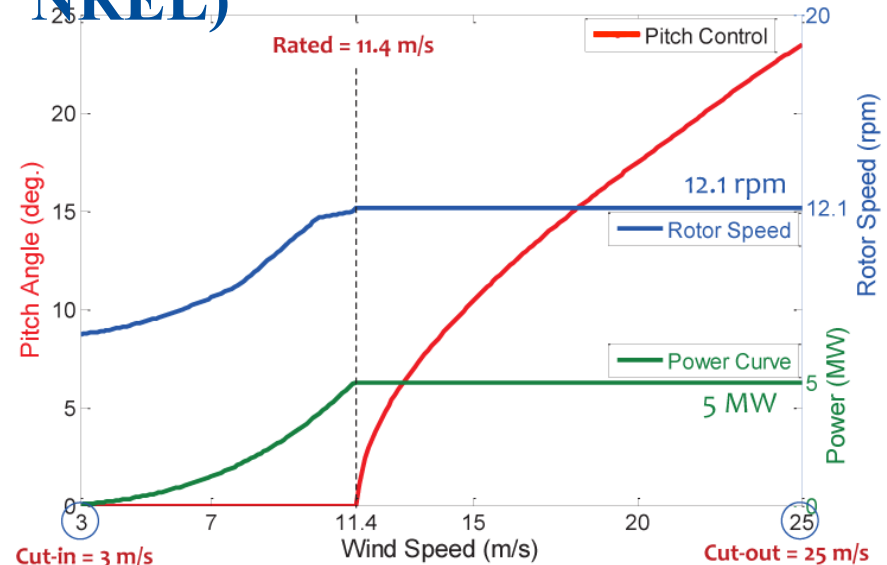


# Aero-hydro-elastic simulations

## 5-MW NREL Baseline turbine model (simulations with FAST, NREL)



(courtesy of NREL)



Above cut-out:  
parked state

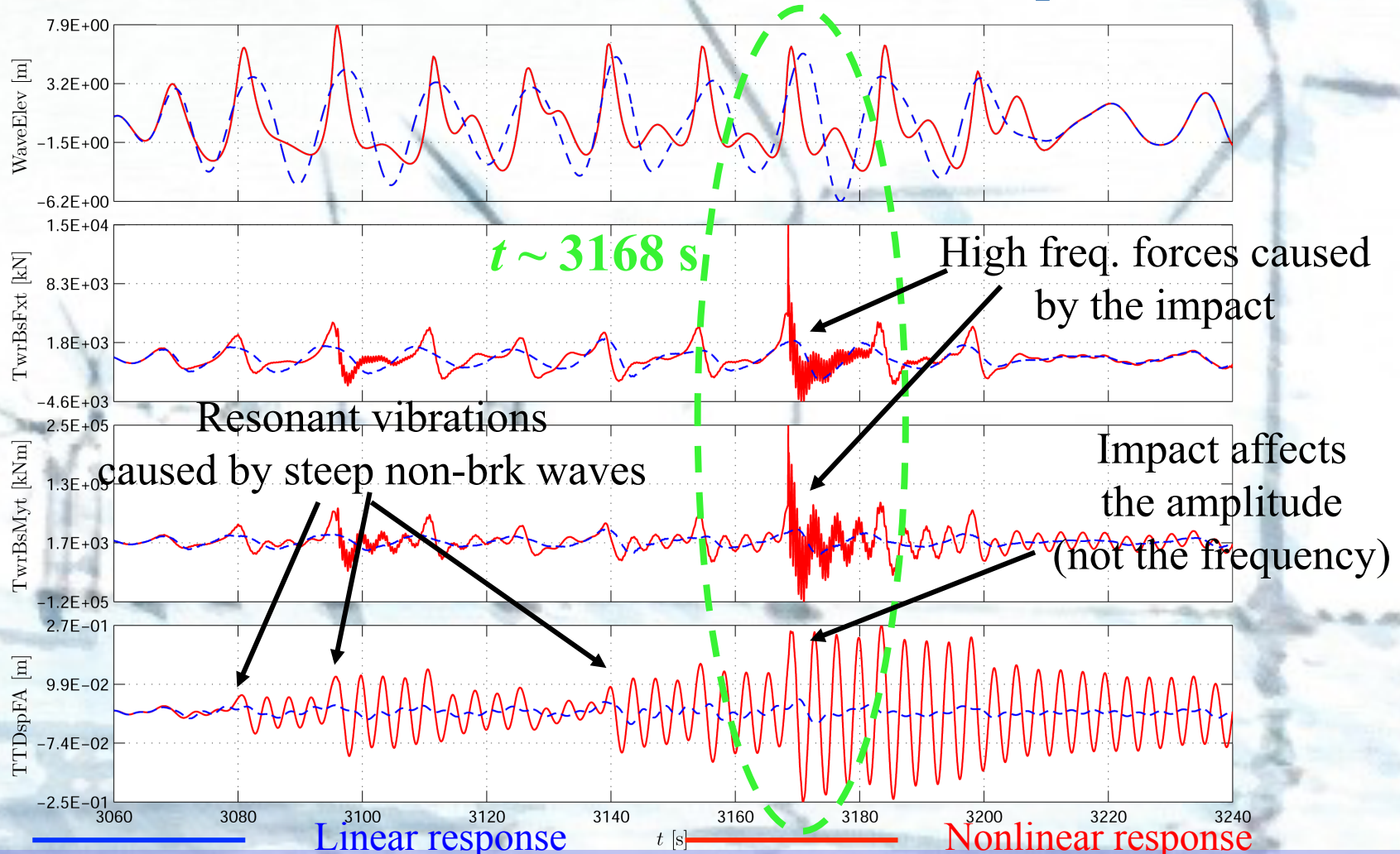
Sea state:

$H_s$ [m]	$T_p$ [s]	HH Wind vel. [m/s]
7.5	15	33

$H_s$ : significant wave height;  $T_p$ : wave spectral peak period

## Aero-hydro-elastic simulations - Tower

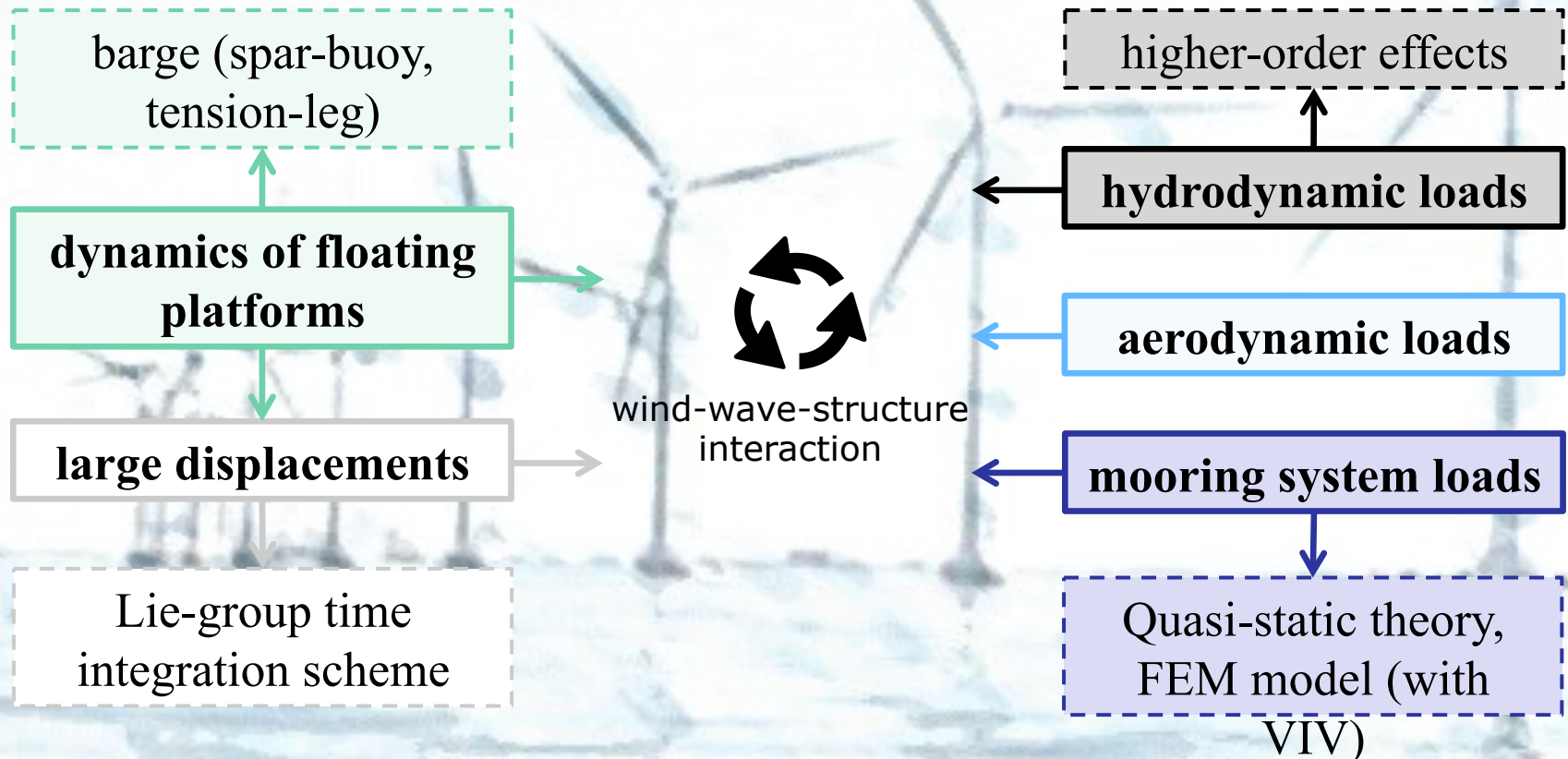
**FNL vs. L wave kinematics and tower response**  $f_{tower} = 0,28 \text{ Hz}$





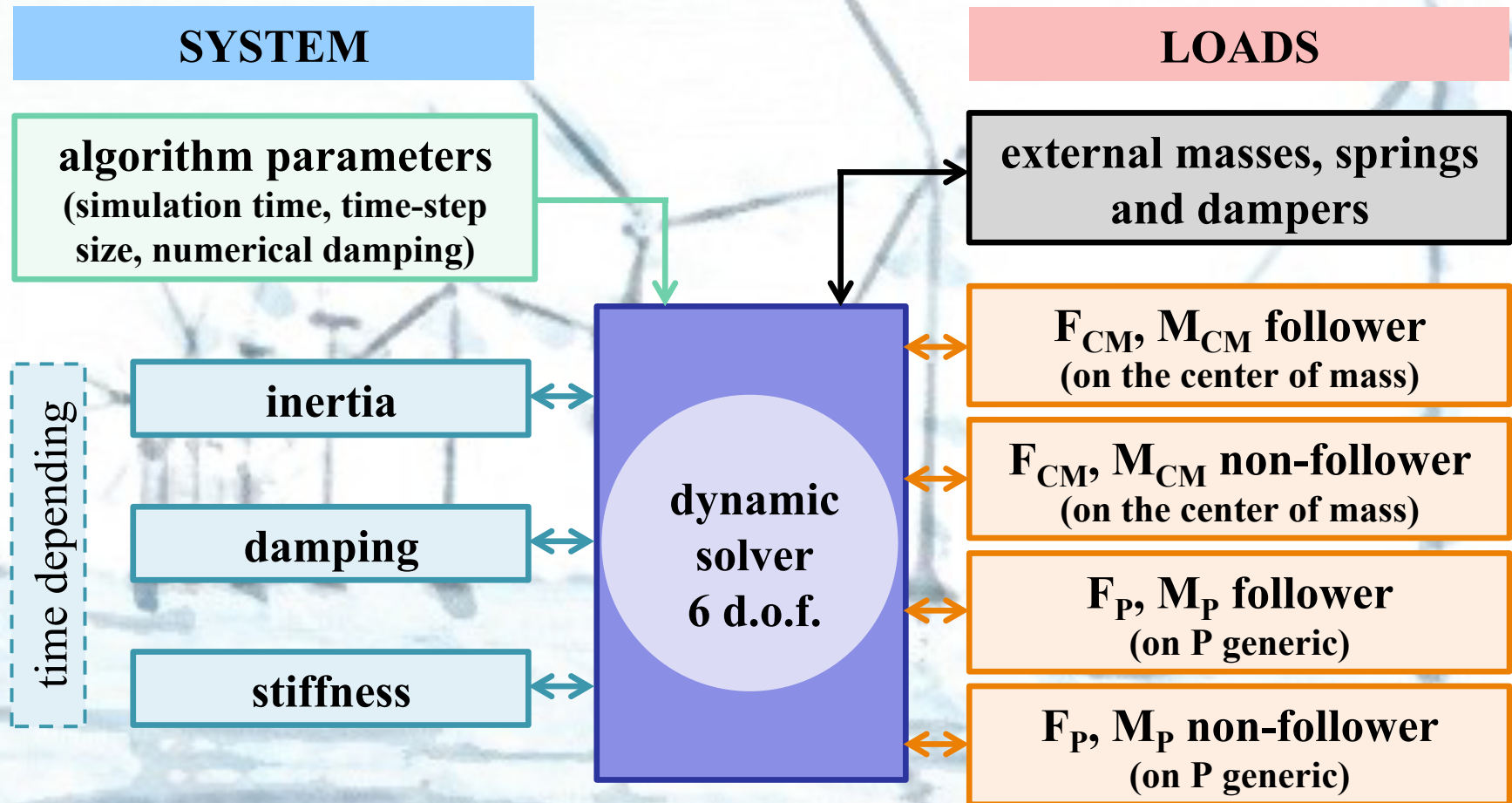
# Floating technologies

## Wind-wave-structure interaction problem



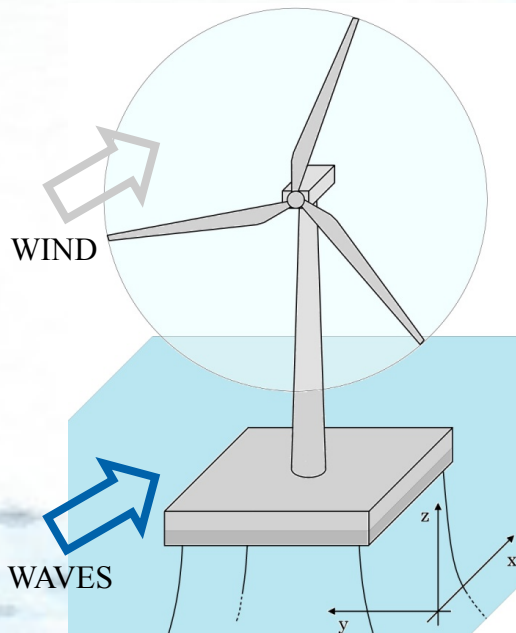
# Floating technologies

## Floating platform dynamics: numerical model



# Floating technologies

## Hydrodynamic problem



- Potential-flow theory
- First-order hydrodynamics, i.e. superimposition of:
  - hydrostatics
  - radiation
  - diffraction

- Coupling with the dynamic solver:
  - configuration-depending loads
  - additional mass, damping and stiffness

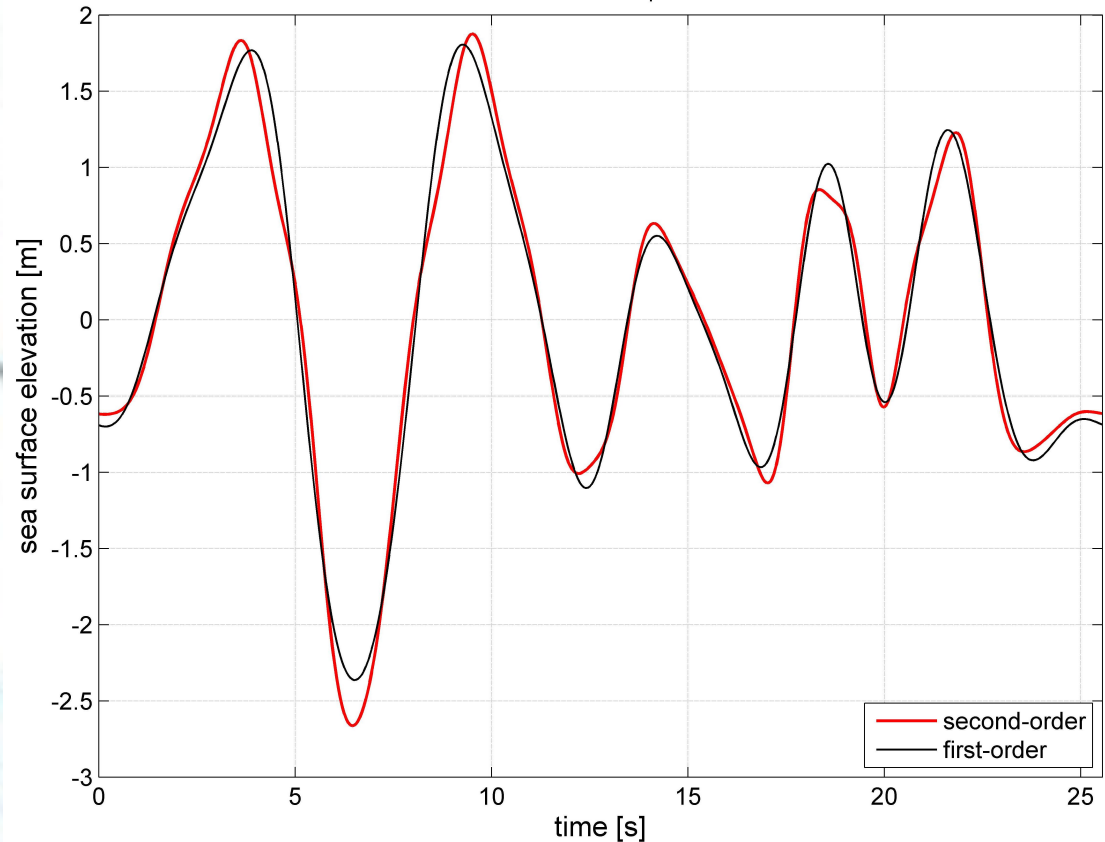
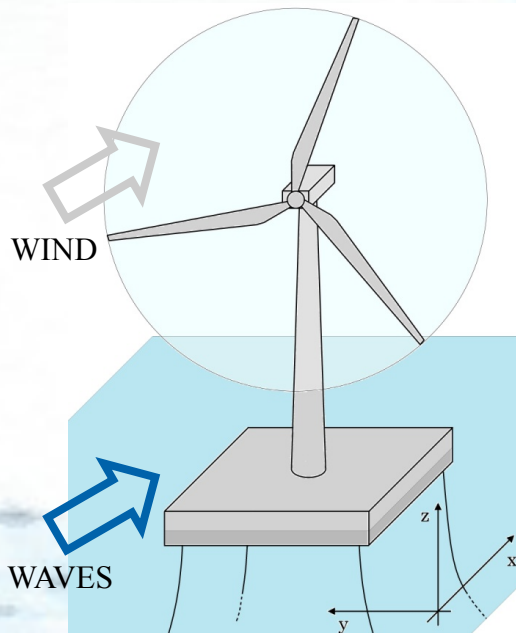
- Higher-order effects (next step)



# Floating technologies

## Hydrodynamic problem

PM-spectrum,  $H_s = 2.25$  m,  $T_p = 7.13$  s,  $\Delta t = 0.05$  s



Comparison between the first-order and the second order wave kinematics (obtained using the same random phases).

# Mooring Lines

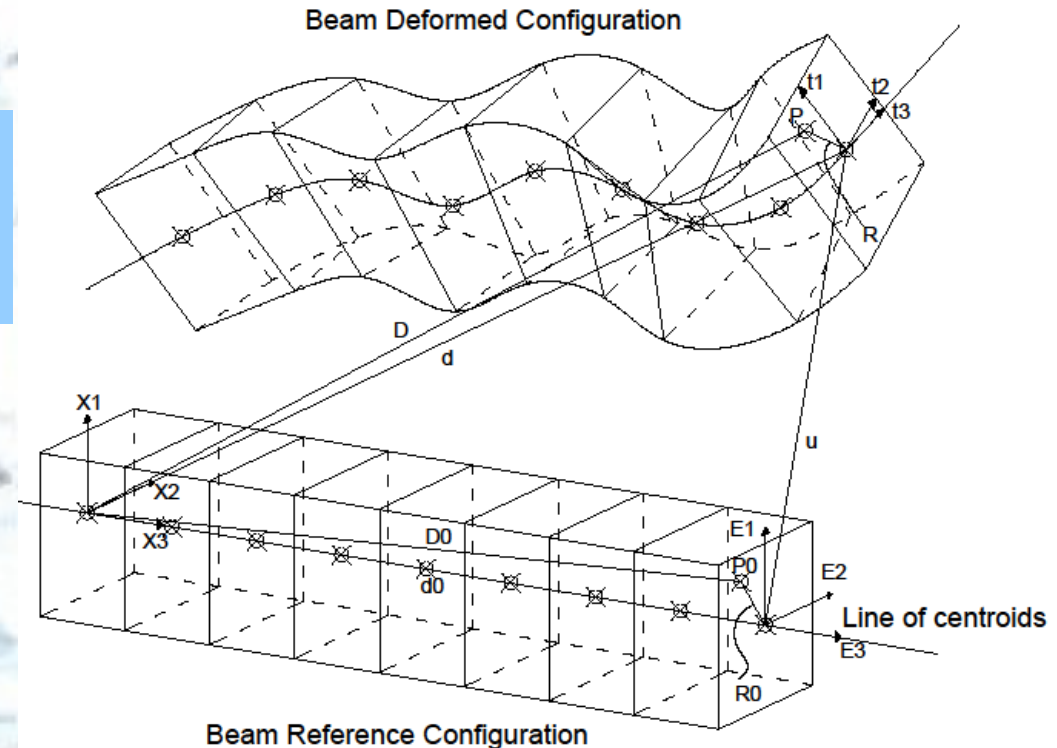
## Structural Dynamics

The dynamics of each mooring line is fully reproduced discretizing the structure with a dynamic finite element technique.

### Structural Model

**Structure discretized with  
Geometrically-exact beam  
elements (SIMO)**

**Time integration performed  
with a generalized-alpha  
method**



# Mooring Lines

## Hydrodynamic Model

### High fidelity model

GLOBAL MODEL OF THE CABLE  
FEM ONLY MODEL

LOCAL MODEL OF THE CABLE  
WITH IMPOSED MOTION  
FEM+CFD MODEL

EXP. MOTION  
IN FULL SCALE

STATISTICAL  
PROPERTIES  
OF THE MOTION

GENERATION OF  
CORRELATED  
RANDOM MOTIONS  
 $u_{x1}(t), u_{y1}(t), u_{x2}(t), u_{y2}(t)$

MEASURED REACTIONS  
 $F_{x1}(t), F_{y1}(t), F_{x2}(t), F_{y2}(t)$

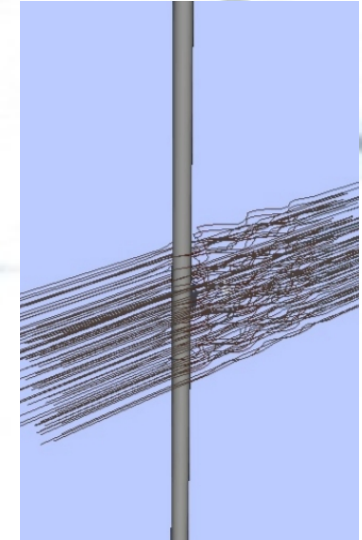
IMPOSED MOTION  
 $u_{x1}(t), u_{y1}(t), u_{x2}(t), u_{y2}(t)$   
 $\dot{u}_{x1}(t), \dot{u}_{y1}(t), \dot{u}_{x2}(t), \dot{u}_{y2}(t)$   
 $\ddot{u}_{x1}(t), \ddot{u}_{y1}(t), \ddot{u}_{x2}(t), \ddot{u}_{y2}(t)$

SYSTEM IDENTIFICATION  
TECHNIQUE

Reduced Order Model

HYDRODYNAMIC FORCES  
AT EACH NODE OF THE FEM  
 $F_{x1}(t), F_{y1}(t), F_{x2}(t), F_{y2}(t)$

MOTION HISTORY  
 $u_{x1}(t), u_{y1}(t), u_{x2}(t), u_{y2}(t)$   
 $\dot{u}_{x1}(t), \dot{u}_{y1}(t), \dot{u}_{x2}(t), \dot{u}_{y2}(t)$   
 $\ddot{u}_{x1}(t), \ddot{u}_{y1}(t), \ddot{u}_{x2}(t), \ddot{u}_{y2}(t)$   
FLOW VELOCITY PROFILE  
 $U(x,t)$



Coupling of a CFD solver  
with a geometrically exact  
FEM solver

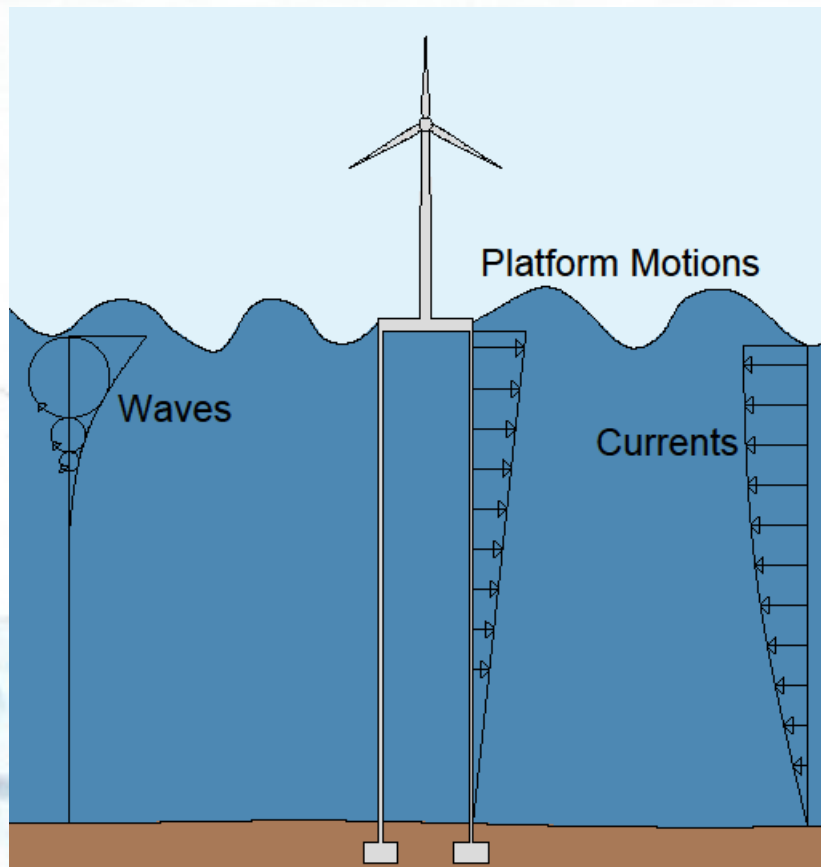
The hydrodynamic model is based on an efficient reduced order model (ROM) suitable for long term simulations in time domain but able to capture complex phenomena such as vortex induced vibrations. Parameters of the model are calibrated using results from high fidelity FSI simulations conducted on a reduced domain size.



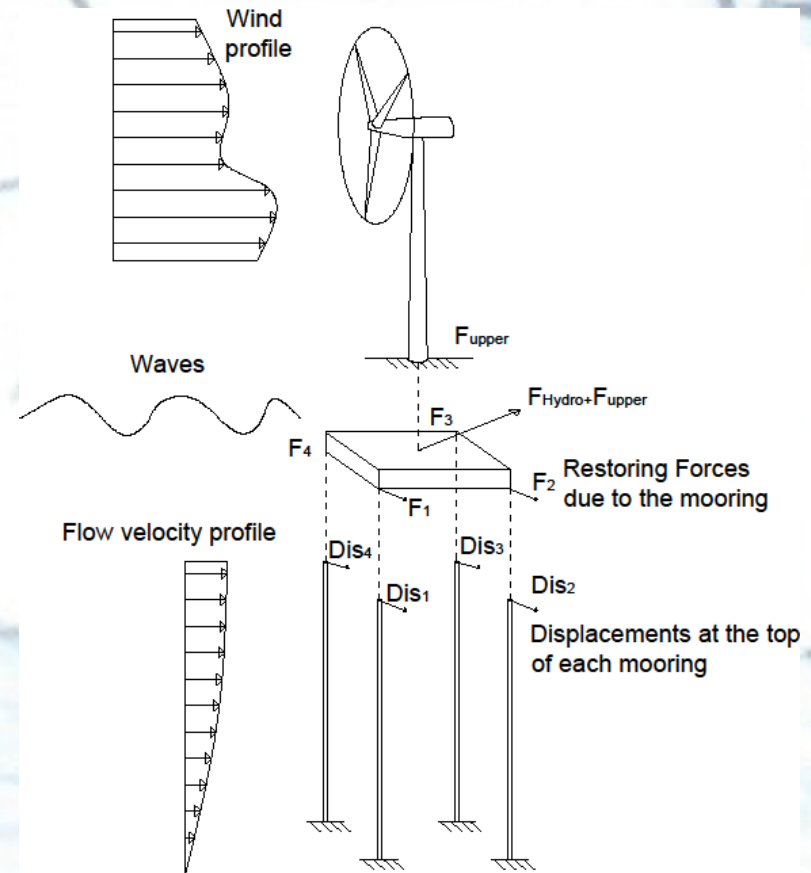
# Mooring Lines

## Coupling with the platform solver

### Actions on the moorings



### Coupling Procedure: Block Gauss-Seidel Algorithm



# Conclusions

## Fixed-bottom substructures

- In severe sea states, resonant vibrations can be triggered by high-order nonlinear waves contributions.
- Such vibrations cannot be captured when the standard linear wave theory is used.

## Floating platforms

- Development of a dynamic solver based on large-displacement approach.
- Cable's loads: from quasi-static theory to ROM for geometrically exact FEM solvers.

# Offshore wind turbines: from fixed-bottom to floating technologies

*by C. Borri, A. Giusti, E. Marino, G. Stabile*

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**Thank you for your kind attention!**